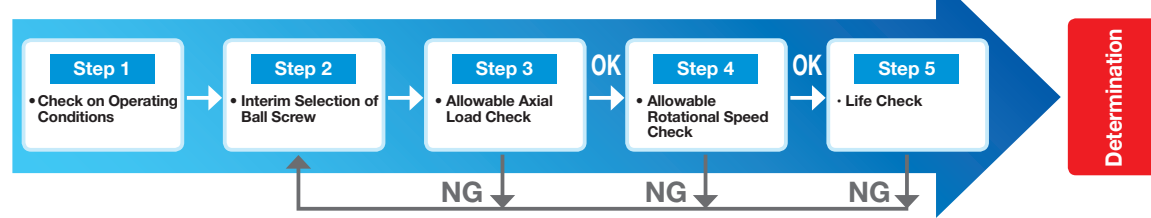


Use the following steps to select a ball screw suited to the usage criteria.



## Step 1 Check on Operating Conditions

Refer to Operating Conditions below.

NO	Item	Unit
①	Positioning Accuracy	mm
②	Stroke	mm
③	Travel Speeds	mm/s
④	Drive Motor Speed	min <sup>-1</sup>
⑤	Weight of Workpiece and Table	Kg
⑥	Mounting Orientation (horizontal or vertical)	-
⑦	Life Hours	Time
⑧	Motion pattern (Duty Cycle Line Diagram) (See Figure 1)	-

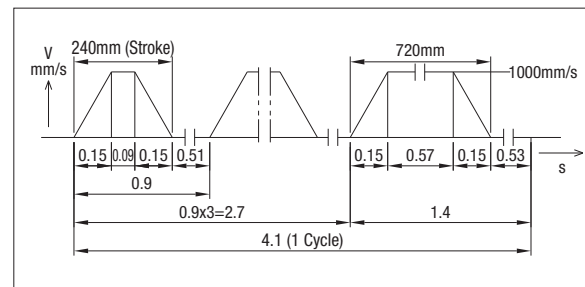


Figure 1 (Ex.) Duty Cycle Line Diagram

## Step 2 Interim Selection of Ball Screw

Consider the applicability of the following items to the conditions confirmed in step 1 and provisionally decide the ball screw.

- Selection of Lead Accuracy of Ball Screws**
  - ① Select the ball screw that satisfies the positioning precision. Check the following two points.  
Lead Accuracy: For details, see P.2223 on the catalog.  
Axial Clearance: For details, see P.2224 on the catalog.
- Selection of Ball Screw Shaft Length**
  - Generally, the shaft length should be ② stroke + shaft end of 50~150 mm + allowance.  
The allowance is to prevent detachment, and one end should be (lead x 1.5~2) mm or more.
- Provisional positioning of lead**
  - ③ Travel speeds, and ④ speed of the drive motor should be used to select the lead.
- Temporary selection of the shaft diameter**
  - ⑤ Weight of work and table, and ⑥ mounting position, and provisionally decided lead should be used to select the shaft diameter.

### <Impact on Positioning Precision of Axial Clearance>

If the ball screw has axial clearance, when positioning operation is performed from the positive direction, because the work does not move even when the screw shaft rotates, a difference occurs in the clearance interval between the theoretical movement amount obtained from the revolution speed of the screw shaft and the actual movement amount.

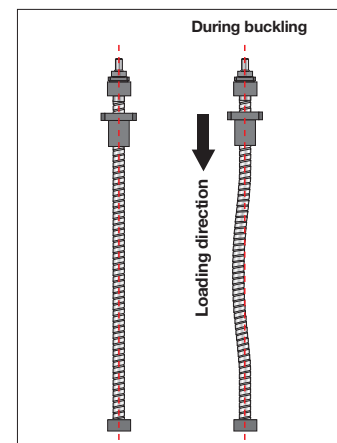
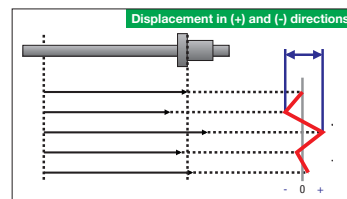


Figure 2 Buckled Ball Screw

## Step 3 Allowable Axial Load Check

The max. axial load to the ball screw must be equal to or less than the allowable axial load value. If a load exceeding the allowable axial loading is applied, it is possible that the ball screw's screw shaft will buckle. (Figure 2)

### Allowable Axial Load

The allowable axial load represents an allowed maximum load, including a safety margin, to prevent shaft buckling from occurrence. The finer the shaft diameter or the longer the shaft the easier it is for buckling to occur.

For details, see P.2225 on the catalog.

## Step 4 Allowable Rotational Speed Check

The rotational speed of the ball screw must be less than the allowable rotational speed. If it exceeds the allowed rotational speed, the thread and the nut will be affected in the following way.

- Screw Shaft:** When the allowable rotational speed is exceeded, resonance will begin at a unique oscillating frequency and this might disable operation. (Figure 3)
- Nut:** If the orbital speed of the steel balls inside the nut becomes large, it is possible that the circulation components will be damaged by the impact force. (Figure 4)

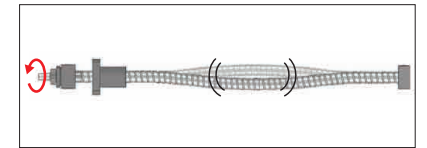


Figure 3 Resonating Ball Screw

### Allowable Rotational Speed

Refers to the allowable rotational speed that is 80% or less of the critical speed that matches the rotational speed of a ball screw at which there is a unique oscillation possessed by the screw shaft. The ball screw rotational speed is decided by the necessary travel speed and ball screw lead.

To decide the allowable rotational speed, it is necessary to consider the following two elements.

- Critical speed for the rotating shaft
- Limit rotational speed of the balls circulating inside the nut

For details, see P.2226 on the catalog.

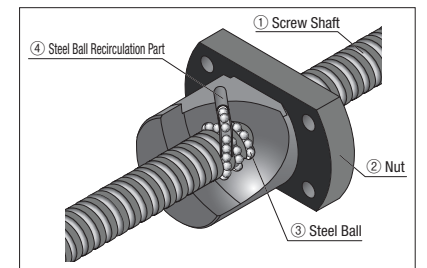


Figure 4 Ball Screw Circulation Structure (Tube Style)

## Step 5 Life Check

In order to use the equipment beyond the expected life, life calculations are required.

### Operating Hours of Ball Screws

This refers to the total revolutions, time, or distance up until chipping begins to occur due to fatigue causes by some kind of repetitive stress on the ball rolling surface or balls. The lifespan of the ball screw is calculated from the basic dynamic load rating. See Figures 5 and 6 for expired parts that have chips.

When a certain group of the same ball screws are operated with a certain axial load and 90% of the screws achieve 1 million rotations (10<sup>6</sup>) without flaking in its operating life, such axial load is defined as a basic dynamic load rating.

For details, see P.2227 on the catalog.



Figure 5 Thread Inside Nut

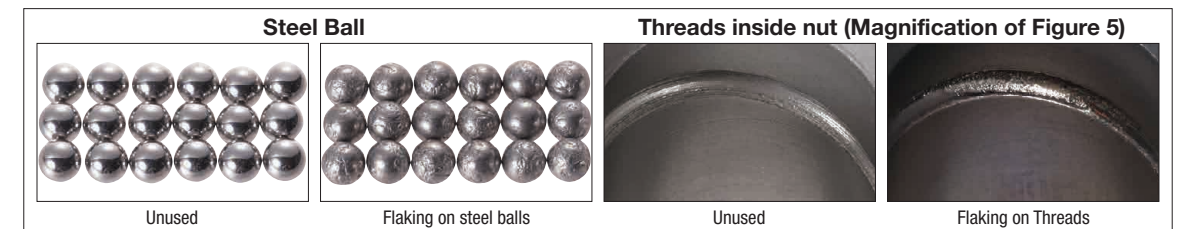
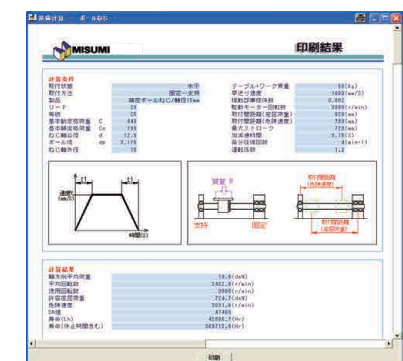
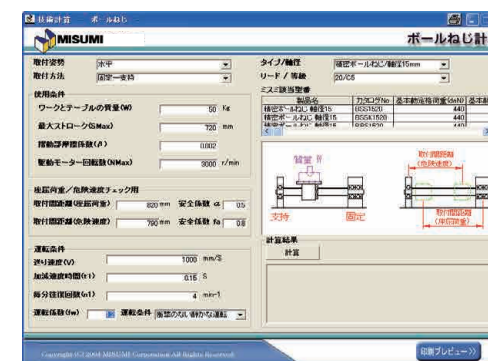


Figure 6 Flaking on Ball Screw Components

When choosing, it is necessary to ensure the temperature impact and rigidity is suitable for the usage environment and selection criteria. For details, see P.2223~2230 of the catalog technical pages and choose a ball screw that is suitable for the purpose of use.

### Overview of MISUMI Technical Calculation Software

Ball screw's Life calculations and safety margin check can be performed just by entering some operation conditions. ([http://download.misumi.jp/mol/fa\\_soft.html](http://download.misumi.jp/mol/fa_soft.html))



# Rolled Ball Screws / Precision Ball Screws

## Lineup

### Ball Screw Lineup

List of Type, Accuracy Grade, Shaft Dia., Lead, Axial Play and Shaft Length of MISUMI Ball Screws

Provisionally select the ball screw suitable for the purpose of use from the list and select the product following the selection procedure on P.681.

#### Rolled Ball Screw Lineup

Type	Standard Type	Shaft Dia.	Lead	Axial Play (mm)	Shaft Length (mm)			
					MIN	MAX		
Existing Product Compact Nut Accuracy Grade C10	BSSC	8	2	0.05 or Less	100	400		
		10	4		150	600		
		12	4		150	800		
		15	5	150	1200			
		20	10	0.10 or Less	200	1200		
		25	5	0.15 or Less	200	2000		
Existing Product Standard Nut Accuracy Grade C10	BSSZ BSSR	8	2	0.05 or Less	100	400		
		10	4		100	380		
		12	4		150	585		
		14	5		150	600		
		15	5		150	585		
		20	10		150	800		
		15	5	0.10 or Less	150	800		
		20	10	0.15 or Less	200	1200		
		25	5	0.10 or Less	200	2000		
		25	10	0.20 or Less	200	2000		
		25	20	0.12 or Less	300	2000		
		28	6	0.10 or Less	250	2000		
		32	10	0.20 or Less	300	2000		
		32	20	0.15 or Less	300	2000		
		C-VALUE Products Standard Nut Accuracy Grade C10	C-BSSC	8	2	0.05 or Less	100	400
				10	4		150	585
				12	5		150	600
				15	5	0.10 or Less	150	800
20	10			0.15 or Less	200	1200		
25	5			0.10 or Less	200	2000		
25	10			0.15 or Less	250	2000		
25	20			0.12 or Less	300	2000		
25	25			0.12 or Less	300	2000		
Existing Product Block Nut Accuracy Grade C10	BSBR			15	5	0.10 or Less	150	1200
				20	10		200	1200
				25	15		200	1500
		15	5	0.15 or Less	150	1200		
		20	10	0.20 or Less	200	1200		
		25	15	0.20 or Less	250	1500		
Existing Product Standard Nut Accuracy Grade C7	BSST	8	2	0.03 or Less	100	380		
		10	4		150	585		
		12	4		150	795		
		15	5		150	1200		
		20	10		200	1200		
		25	5		200	1200		
		20	10	0.05 or Less	250	2000		
		25	5	0.03 or Less	200	2000		
		25	10	0.07 or Less	300	2000		

#### Precision Ball Screw Lineup

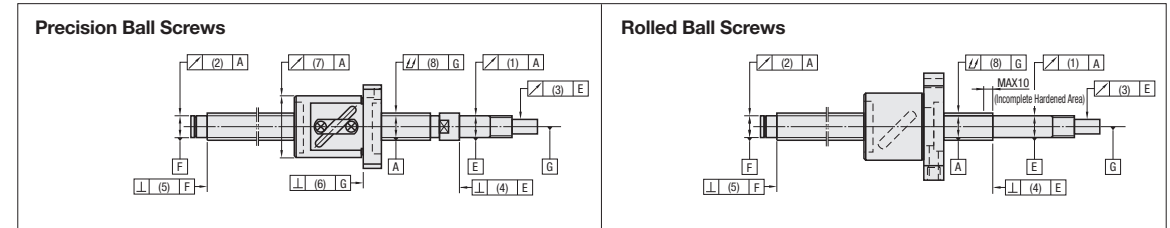
Type	Standard Type	Shaft Dia.	Lead	Axial Play (mm)	Shaft Length (mm)			
					MIN	MAX		
Existing Product Standard Nut Accuracy Grade C5	BSS	8	2	0.005 or Less	100	210		
		10	4		100	315		
		12	4		150	380		
		15	5		150	450		
		20	10		150	400		
		25	5		150	450		
		10	4	0.008 or Less	150	380		
		12	5	0.008 or Less	150	445		
		15	10	0.008 or Less	200	1095		
		20	5	0.008 or Less	200	1000		
		20	10	0.008 or Less	250	1500		
		25	5	0.008 or Less	300	995		
		25	10	0.008 or Less	300	1500		
		25	20	0.008 or Less	300	1500		
		C-VALUE Standard Nut Accuracy Grade C5	C-BSS	8	2	0.015 or Less	100	210
				10	4		100	315
				12	4		150	380
				15	5		150	445
20	10			150	450			
25	5			150	450			
15	10			0.015 or Less	200	1095		
20	5			0.015 or Less	200	1095		
20	10			0.015 or Less	250	1500		
25	5			0.015 or Less	300	995		
25	10			0.015 or Less	300	1500		
Existing Product Standard Nut Accuracy Grade C3	BSX			6	1	0 (Preloaded)	80	205
		8	1	80	255			
		10	2	100	240			
		12	2	100	310			
		15	2	150	390			
		25	5	150	440			
Existing Product Standard Nut Accuracy Grade C7	BSSE	8	2	0.030 or Less	100	210		
		10	4		100	315		
		12	4		150	380		
		15	5		150	445		
		20	10		150	450		
		25	5		150	450		
		10	4	0.030 or Less	200	600		
		12	5	0.030 or Less	150	1095		
		15	10	0.030 or Less	200	1095		
		20	5	0.030 or Less	200	1095		
		20	10	0.030 or Less	250	1500		
		25	5	0.030 or Less	250	1500		
		25	10	0.030 or Less	300	1500		
		25	20	0.030 or Less	300	1500		

#### Meaning of Terms

- Accuracy Grade** Lead Accuracy of Ball Screws defined by JIS Standards. Smaller numbers mean higher lead precision.
- Shaft Dia.** Screw O.D.
- Lead** Refers to the distance a nut moves when the screw shaft makes a full rotation.
- Axial Play** Axial play between the screw shaft and nuts.

## Mounting Interface Accuracies

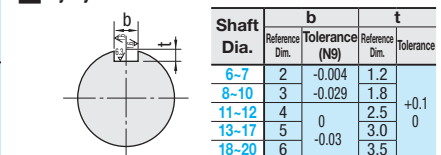
### Mounting Interface Accuracies



Unit: mm

Part Number	Type	Screw Shaft O.D.	(1) (2)	(3)	(4) (5)	(6)	(7)
			Run-out Tolerance (Max.)	Run-out Tolerance (Max.)	Perpendicularity Tolerance (Max.)	Perpendicularity Tolerance (Max.)	Run-out Tolerance (Max.)
BSX	BSX	6	0.008	0.008	0.004	0.008	0.008
		8					0.010
		10					0.010
		12					0.012
BSS C-BSS	BSS C-BSS	8	0.011	0.011	0.005	0.010	0.012
		10					0.015
		12					0.012
		15					0.012
		20					0.013
BSSE BSST	BSSE BSST	8	0.014	0.014	0.007	0.014	0.020
		10					0.030
		12					0.020
		15					0.020
		20					0.020
BSSR BSSZ BSSC C-BSSC	BSSR BSSZ BSSC C-BSSC	8	0.040	0.040	0.010	-	-
		10					
		12					
		14					
		15					
		20					
		25					
		28					
		32					
		32					
BSBR	BSBR	15	0.040	0.040	0.010	-	-
		20					
		25					
		25					

#### Keyway Dimension Details Located at P on Fixed Side Shaft End



Unit: mm

Part Number	Type	Screw Shaft O.D.	(8) Run-out Tolerance (Max.)										
			Screw Shaft Length										
			~125	126~200	201~315	316~400	401~500	501~630	631~800	801~1000	1001~1250	1251~1600	1601~2000
BSX	BSX	6	0.025	0.035	0.050	-	-	-	-	-	-	-	-
		8			0.040	0.050	0.065	-	-	-	-	-	
		10			0.040	0.050	0.065	-	-	-	-	-	
		12			0.040	0.050	0.065	-	-	-	-	-	
BSS C-BSS	BSS C-BSS	15	0.035	0.040	0.050	0.065	0.080	0.090	-	-	-	-	-
		8			0.045	0.055	0.060	0.075	0.090	0.120	0.150	0.190	-
		10			0.045	0.055	0.060	0.075	0.090	0.120	0.150	0.190	-
		12			0.045	0.055	0.060	0.075	0.090	0.120	0.150	0.190	-
		20			0.045	0.055	0.060	0.075	0.090	0.120	0.150	0.190	-
BSSE BSST	BSSE BSST	25	0.060	0.075	0.100	-	-	-	-	-	-	-	-
		8			0.055	0.065	0.080	0.100	0.120	0.150	-	-	-
		10			0.055	0.065	0.080	0.100	0.120	0.150	-	-	-
		12			0.055	0.065	0.080	0.100	0.120	0.150	-	-	-
		15			0.055	0.065	0.080	0.100	0.120	0.150	-	-	-
BSSR BSSZ BSSC BSBR C-BSSC	BSSR BSSZ BSSC BSBR C-BSSC	20	0.100	0.140	0.210	(0.270)	-	-	-	-	-	-	-
		8			0.060	0.075	0.100	-	-	-	-	-	-
		10			0.060	0.075	0.100	-	-	-	-	-	-
		12			0.060	0.075	0.100	-	-	-	-	-	-
		15			0.060	0.075	0.100	-	-	-	-	-	-
		20			0.060	0.075	0.100	-	-	-	-	-	-
		25			0.060	0.075	0.100	-	-	-	-	-	-
		28			0.060	0.075	0.100	-	-	-	-	-	-
		32			0.060	0.075	0.100	-	-	-	-	-	-
		32			0.060	0.075	0.100	-	-	-	-	-	-

# Rolled Ball Screws / Precision Ball Screws

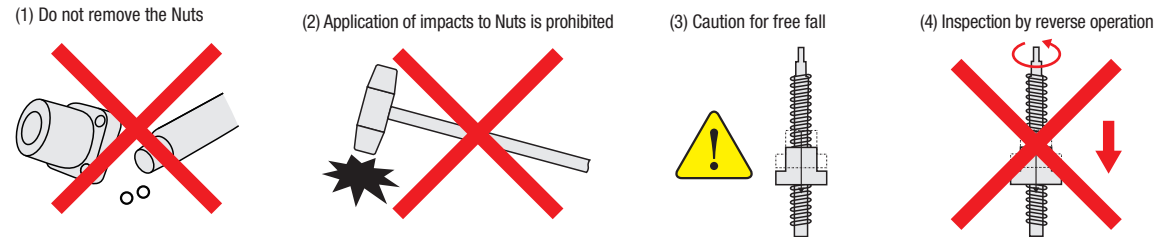
## Precautions on Handling

## Lubrication, Grease Measures, Cautions on Designing and Assembling Peripherals

### Precautions on handling Ball Screws

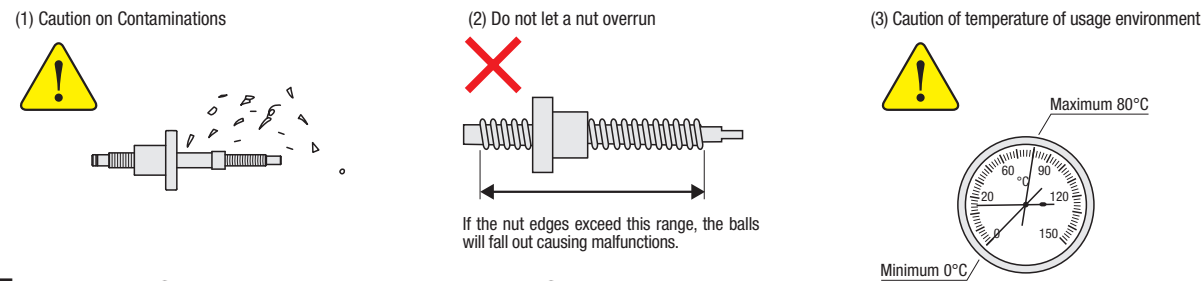
#### Precautions on Handling

- Removing the ball nut from the screw shaft causes the ball to fall out rendering the ball screw unusable. Do not disassemble Ball Screws. It may attract dusts and degrade assembly accuracy. Use dedicated temporary shafts when removing Ball Nuts.
- Do not give an external impact to a screw shaft outer diameter, thread and recirculation parts. It may cause recirculation failure and a malfunction.
- Do not tilt the ball screw assembly since a ball screw nut may spin off from a screw shaft due to its own weight. Especially when using a ball screw vertically, place a fall-off prevention mechanism since a ball screw nut may spin off due to its own weight.
- When inspecting the sliding, fix the nut and cause the shaft to rotate, or fix the shaft and cause the nut to rotate.



#### Cautions on use

- Use Ball Screws in clean environments. Use covers, etc. to prevent intrusion of dusts and chips that may cause damages and performance degradations to ball recirculation components.
- Do not let a ball screw nut overrun. It may cause the balls to fall out or damage the ball recirculation parts.
- Avoid using Ball Screws at a temperature of more than 0~80°C. It may damage recirculation parts or seal parts.
- Do not misalign or tilt ball screws shaft support side and a ball screw nut. Life hours may become extremely short due to an offset load to a ball screw nut. When using Support Units, refer to P.760.



### Rolled Ball Screws · About Removing Ball Screws

If the nut is removed from the shaft, the balls contained in the nut will fall out and the ball screw will become unusable. Use dedicated temporary shafts when removing Ball Nuts. MISUMI provides various temporary shafts as option. To order a dedicated temporary shaft together with Ball Screws, add alterations code "TAS" to the end of a part number. **⊗** Nuts cannot be removed using the temporary shafts with Precision Ball Screw BSX, C-BSS, Rolled Ball Screw C-BSSC.

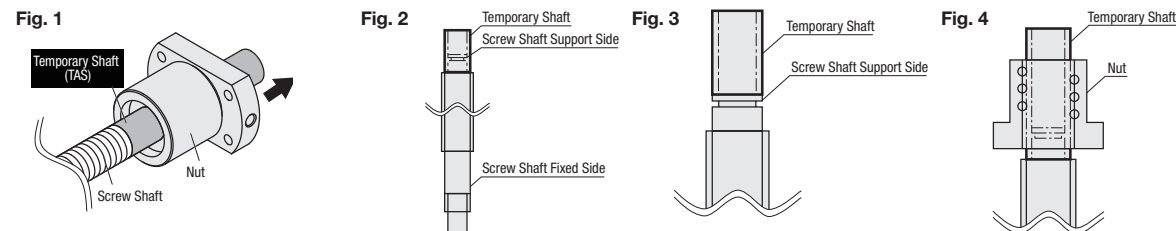
Alterations	Part Number	L	F	P	(TAS)
	BSSZ1510	300			TAS
	BSSR2005	700	F30	P12	TAS

#### Caution on use of Temporary Shaft

- When Taking Out Ball Screws Nut from Screw Shaft
- Stand a screw shaft vertically and place a temporary shaft to the screw shaft support side edge in consistent with screw shaft center. (Refer to Fig. 2)<sup>(\*)</sup>
  - Lightly rotate the nut and install it onto the temporary shaft. (Refer to Fig. 4)
  - After confirming that both nut edges are on the temporary shaft, take out the temporary shaft from the screw shaft.
  - Store the assembly while ensuring that the nut does not fall off of the temporary shaft.

- When Installing Ball Screws Nut to Screw Shaft
- Stand a ball screw shaft vertically and place a temporary shaft to the screw shaft support side edge in consistent with screw shaft center.
  - Rotate the nut with pressing the screw shaft lightly and install it into the shaft.
  - In case there is any interference, do not insert the ball screw forcibly. Try reassembling.

(\*) In BSSZ, BSSR0802, BSSR0804, BSSR1002, BSSR2510, BSST0802 and BSST2510, the screw shaft support side and the temporary shaft are placed as shown in the following Figure 3. Since TAS is unstable, grip TAS firmly from the above until the installation is finished.



### Lubrication (grease inspection and replenishment)

The grease forms an oil film on the ball screw's screw shaft, rolling surface inside the nut, and surface of the balls and acts to reduce friction and prevent heat damage. MISUMI ball screws are filled with grease before shipping, however after commencing use, it is necessary to perform regular and appropriate inspection and grease replenishment. When adding grease, use the same grease that was used at shipment and do not mix with other greases.

#### Guides for inspection and grease replenishment

After 2~3 months of operation, if the grease is very dirty, we recommend to remove the old grease and fill with new grease. Subsequent inspection intervals are recommended to be every 6 months, however, we recommend this timing be adjusted to an interval appropriate for the usage environment.

#### Available Grease

Ball screw products are shipped with grease filled. If not otherwise indicated, lithium soap based grease (Alvania Grease S2 made by Showa Shell Sekiyu K.K) is the standard type that is used. (BSX0601, BSX0801, and BSX0802 are filled with Multemp Grease PS2 made by Kyodo Yushi Co., Ltd.) Grease type can be changed from the standard to the following types.

Part Number	Product Name	Main Features
● L Type	ET-100K (Made by Kyodo Yushi)	Excels in heat resistance, oxidation stability, adhesion and adhesive power. In addition, splash or leakage is little.
● G Type	LG2 (Made by NSK Ltd.)	Special grease for linear guides, ball screws and etc. for clean-room use.

Item	Condition	Unit	Measurement Method	Standard	L Type	G Type
Grease Performance	Thickener	-	-	Lithium Type	Aromatic Diurea	Lithium Type
	Base Oil	-	-	Mineral Oil	Ether Synthetic Oil	Mineral Oil + Synthetic Hydrocarbon Oil
	Base Oil Viscosity	40°C	mm <sup>2</sup> /s	JIS K2220 5.19	131	103
	Viscosity	100°C	-	-	12.2	12.8
	Worked Penetration	-	-	JIS K2220 5.3	283	207
	Dropping Point	-	°C	JIS K2220 5.4	181	<260
	Evaporation Amount	99°Cx22h	wt%	-	-	0.15%
	Oil Separation Rate	100°Cx24h	wt%	JIS K2220 5.14	2.8%	1.2%
	Operating Temp.	In Air	°C	-	-25~+135	-40~200
						-10~80

- ⊗ Usage temperature is for grease performance and not the usable temperature of the ball screw.
- ⊗ Avoid using Ball Screws at a temperature of more than 0~80°C.

#### Available Ball Screws and Grease Types

Type	Accuracy Grade	Type	Unit Price (Add to the price of Standard Type)
Precision Ball Screws	C 5	BSS	● L Type ● G Type
	C 7	BSSE	
	C 7	BSST	● L Type ● G Type
Rolled Ball Screws	C10	BSSR BSSZ	● L Type ● G Type
		BSSRK BSSZK	

⊗ Not applicable to Precision Ball Screw BSX, C-BSS, Rolled Ball Screw BSSC and C-BSSC.

Ordering Example

Part Number - L

● BSS2010L - 700 (L Type Greased)

● BSS2010G - 700 (G Type Greased)

⊗ Please add L or G after the part number of standard type when placing an order.

### Design of Ball Screws and Peripherals, Caution when Assembling

Ball screws are parts that receive only axial load, when a radial load or moment load is received, it could cause sliding failure, vibration/abnormal noise and reduction in lifespan. To prevent parallelism error and misalignment of peripherals that causes radial load and moment load on ball screws, it is important to appropriately design and assemble peripherals.

#### Misalignment of Ball Screw and Support Unit (Figure 1)

- Misalignment occurs when the shaft center of the ball screw fixed to the fixed-side support unit is misaligned with the center of the shaft bearing of the support unit on the support side.
- Misalignment allowance value (reference)
- 20μ or Less
- When there is high precision usage criteria or when using preloaded ball screws, keep the value as low as possible.

#### Parallelism of ball screw and linear guide (Figure 2)

- Parallelism error is where the ball screw is tilting toward up/down or left/right with respect to the linear guide or other references.
- Tilting allowable value (reference) (Figure 3)
- 1/2000 or Less
- When there is high precision usage criteria or when using preloaded ball screws, keep the value as low as possible.

#### Caution During Design

- Design/machining precision of ball screw peripherals can be factors that cause misalignment and tilting. Particularly be cautious of the following two points.
- Flatness of base plate
- Dimensional precision from edge of support unit to shaft center

#### Precautions on Installation

- Mounting/assembly of ball screw peripherals can cause misalignments and tilting. Particularly be cautious of the following four points.
- Error in left/right direction of support unit (Figure 1)
- Parallelism error of linear guide and ball screw (Figure 2)
- Fixing of table and nut bracket
- Fixing of ball screw nut and nut bracket
- If abnormal noise/sliding is being caused by the ball screw movement after assembly, loosen each of the fastened parts again and reassemble while ensuring smooth sliding.

Figure 1 Misalignment of Ball Screw and Support Unit

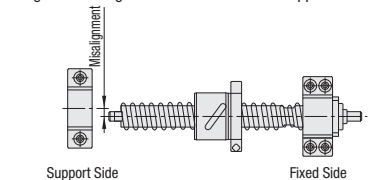


Figure 2 Parallelism Error of Linear Guide and Ball Screw

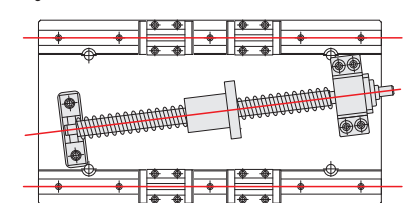
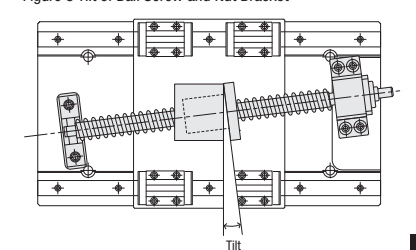


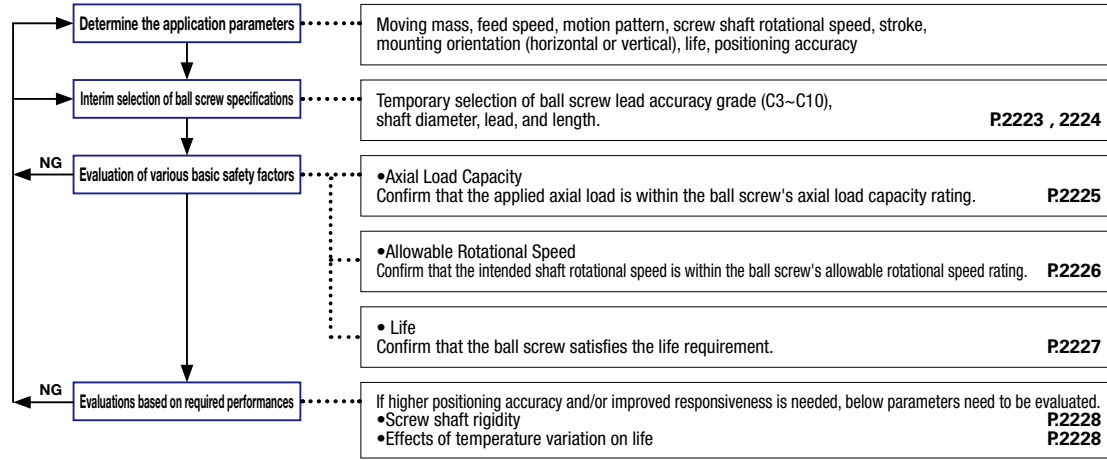
Figure 3 Tilt of Ball Screw and Nut Bracket



# [Technical Data] Selection of Ball Screws 1

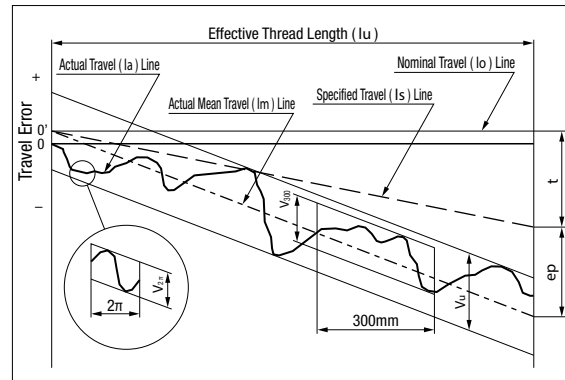
## 1. Ball Screw Selection Procedure

Basic ball screw selection procedure and required evaluation items are shown below.



## 2. Ball Screw Lead Accuracy

Ball screw lead accuracy is defined by JIS Standards property parameters (ep, Vu, V300, V2π). Parameter definitions and allowable values are shown below. In general, a ball screw lead accuracy grade is selected by evaluating if the Actual Mean Travel Error of a candidate is within the allowable positioning error.



Terms	Symbols	Meaning
Actual Mean Travel Error	ep	A value that is Specified Travel subtracted from Actual Mean Travel.
Variation	V <sub>u</sub>	The maximum difference of the actual travel contained between two lines drawn parallel to the actual mean travel, and is defined by three parameters below.
	V <sub>300</sub>	Variation for the effective thread length of screw shaft.
	V <sub>2π</sub>	Variation for an arbitrarily taken length of 300mm within the effective thread length of screw shaft.
Specified Travel	l <sub>s</sub>	Axial travel compensated for temperature rise and loading conditions, in relation to the Nominal Travel (Lead).
Specified Travel Target Value	t	A value that is Nominal Travel subtracted from Specified Travel, over the effective thread length. This value is set to compensate for possible screw shaft expansion and contraction due to temperature changes and applied loads. The value is to be determined based on experiments or experiences.
Actual Travel	l <sub>a</sub>	Actually measured travel distance
Actual Mean Travel	l <sub>m</sub>	A straight line representing the actual travel trend. A straight line obtained by the least-squares method or other approximation methods from the curve representing the actual travel.

Table 1. Positioning Screw (C Class) Actual Mean Travel Error (±ep) and Variation (V<sub>u</sub>) allowances Unit: μm

Thread Effective Length (mm)	Accuracy Grade	Accuracy Grade			
		C3		C5	
over	or less	Actual Mean Travel Error	Variation	Actual Mean Travel Error	Variation
315	400	12	8	23	18
400	500	13	10	25	20
500	630	15	10	27	20
630	800	16	12	30	23
800	1000	18	13	35	25
1000	1250	21	15	40	27
1250	1600	24	16	46	30
		29	18	54	35

Table 2. Positioning Screws (C Class) variation per 300mm (300) Variation per rotation (2π) standard values Unit: μm

Accuracy Grade	C3		C5	
Parameters	V <sub>300</sub>	V <sub>2π</sub>	V <sub>300</sub>	V <sub>2π</sub>
Standard Values	8	6	18	8

Table 3. Transfer Screw (Ct Class) variation per 300mm (V<sub>300</sub>) Standards Unit: μm

Accuracy Grade	Ct7	Ct10
V <sub>300</sub>	52	210

Actual Mean Travel Error (ep) for Transfer Screws (Ct Class) is calculated as ep=2·L<sub>e</sub>/300·V<sub>300</sub>

## 3. Axial Clearances of Ball Screws

Axial clearance does not affect positioning accuracy if the feed is unidirectional, but will generate backlash and negatively affect on positioning accuracy if the direction of the axial load is reversed. Select the axial clearance in such a way that the current requirement for positioning accuracy are met.

Table 4. Axial Clearances of Rolled Ball Screws

Types	Prod. Example	Screw Shaft Dia.	Lead	Axial Clearance (mm)	Screw Shaft Length (mm)			
					MIN	MAX		
Existing Products Compact Nut Accuracy Grade C10	BSSC	8	2	0.05 or less	100	400		
					150	600		
		10	4		150	800		
					150	1200		
		15	5		200	1200		
					200	2000		
20	10	250	2000					
		200	2000					
Existing Products Standard Nut Accuracy Grade C10	BSSZ BSSR	8	2	0.05 or less	100	400		
					100	380		
		10	4		150	585		
					150	600		
		12	4		150	585		
					150	800		
		14	5	150	800			
				150	1200			
		15	10	200	1200			
				200	1200			
		20	5	200	2000			
				200	2000			
		25	10	250	2000			
				250	2000			
		28	6	250	2000			
				300	2000			
		32	10	300	2000			
				300	2000			
C-VALUE Products Standard Nut Accuracy Grade C10	C-BSSC	8	2	0.10 or less	100	400		
					150	585		
		10	4		150	600		
					150	800		
		12	5		150	800		
					150	1200		
		15	10	200	1200			
				200	1200			
		20	5	200	2000			
				200	2000			
		25	10	250	2000			
				250	2000			
		28	10	300	2000			
				300	2000			
		32	10	300	2000			
				300	2000			
		Existing Products Block Nut Accuracy Grade C10	BSBR	15	5	0.10 or less	150	1200
							200	1200
20	10			200	1500			
				200	1500			
25	10			200	1200			
				200	1200			
25	10	200	1500					
		200	1500					
Existing Products Standard Nut Accuracy Grade C7	BSST	8	2	0.03 or less	100	380		
					150	585		
		10	4		150	795		
					150	1200		
		15	5		200	1200		
					200	1200		
		20	10	200	1200			
				200	1200			
		25	5	200	2000			
				200	2000			
		25	10	250	2000			
				250	2000			

Table 5. Axial Clearances of Precision Ball Screws

Types	Prod. Example	Screw Shaft Dia.	Lead	Axial Clearance (mm)	Screw Shaft Length (mm)			
					MIN	MAX		
Existing Products Standard Nut Accuracy Grade C5	BSS	8	2	0.005 or less	100	210		
					100	315		
		10	4		150	380		
					150	450		
		12	5		150	445		
					150	400		
		15	10		150	450		
					200	600		
		20	5		150	1095		
					200	1095		
		25	10		230	1095		
					250	1000		
C-Value Standard Nut Accuracy Grade C5	C-BSS	8	2	0.008 or less	100	210		
					100	315		
		10	4		150	380		
					150	445		
		12	5		150	450		
					200	600		
		15	10	150	1095			
				200	1095			
		20	5	230	1095			
				250	1000			
		25	10	200	1500			
				250	1500			
		Existing Products Standard Nut Accuracy Grade C3	BSX	6	1	0 (Preloaded)	80	205
							80	255
				8	2		100	240
							100	310
				10	2		150	390
							150	440
15	5	150	590					
		150	590					
Existing Products Standard Nut Accuracy Grade C7	BSSE	8	2	0.030 or less	100	210		
					100	315		
		10	4		150	380		
					150	445		
		12	5		150	450		
					200	600		
		15	10		150	1095		
					200	1095		
		20	5		230	1095		
					200	1000		
		25	10		250	1500		
					300	1500		

### Selection Example of Lead Accuracy

- <Requirements>
- Ball screw diameter Ø15, lead 20.
  - Stroke 720mm
  - Positioning accuracy ±0.05mm/720mm

<Selection Details>  
Select an appropriate lead accuracy grade based on the application requirements.

- Evaluating the screw thread length  
Stroke+Nut Length+Margin=720+62+60=842  
\*The Margin shown above is an overrun buffer, and normally determined as 1.5~2 times the screw lead.  
Lead 20x1.5x2 (both ends)=60
- Evaluating the lead accuracy  
Verify the actual mean travel error ±ep for 842mm ball screw thread by referencing the Table 1. on P.2223.  
C3 ... ±0.021mm/800~1000mm  
C5 ... ±0.040mm/800~1000mm
- Determining the lead accuracy  
It can be determined that a C5 grade (±0.040/800~1000mm) ball screw can satisfy the required positioning accuracy of ±0.05/720mm.

### Selection Example of Axial Clearance

- <Requirements>
- Ball screw diameter Ø15, lead 5.
  - Allowable backlash ±0.01mm

<Selection Details>  
From Table 5., it can be determined that C5 grade with 0.005mm or less axial clearance satisfies the allowable backlash amount of 0.01mm for the Ø15 group.

# [Technical Data] Selection of Ball Screws 2

## 4. Allowable Axial Load

Allowable Axial Load is a load with a safety margin built-in against a shaft buckling load. Axial load that applies to a ball screw needs to be less than Allowable Maximum Axial Load. Allowable Axial Load can be obtained by the following formula. Additionally, approximate Allowable Axial Load can be obtained from Table 1. Allowable Axial Load Graph.

### •Allowable Axial Load (P)

$$P = \frac{n\pi^2 EI}{\ell^2} \alpha = m \frac{d^4}{\ell^2} \times 10^4 (\text{N})$$

Where:

P: Allowable Axial Load (N)

ℓ: Distance between Points of Buckling Load (mm)

E: Young's Modulus (2.06×10<sup>11</sup>N/mm<sup>2</sup>)

I: Min. Geometrical Moment of Inertia of Across Root Thread Area (mm<sup>4</sup>)

$$I = \frac{\pi}{64} d^4$$

d : Thread Root Diameter (mm)

n, m : Coefficient Determined by Method of Screw Support

Method of Screw Support	n	m
Support - Support	1	5
Fixed - Support	2	10
Fixed - Fixed	4	19.9
Fixed- Free	0.25	1.2

α : Safety Factor = 0.5

For higher safety, a higher safety factor should be required.

### Allowable Axial Load Calculation Example

Find the Allowable Axial Load for Fig.1

<How to use>

- Thread shaft diameter Ø15, Lead 5
- Mounting method Fixed - Support
- Distance between Points of Buckling Load ℓ: 820mm
- Screw Shaft Root Diameter d 12.5

<Calculations>

g=15.1 since the mounting method is Fixed-Supported, the Allowable Rotational Speed (Nc) is,

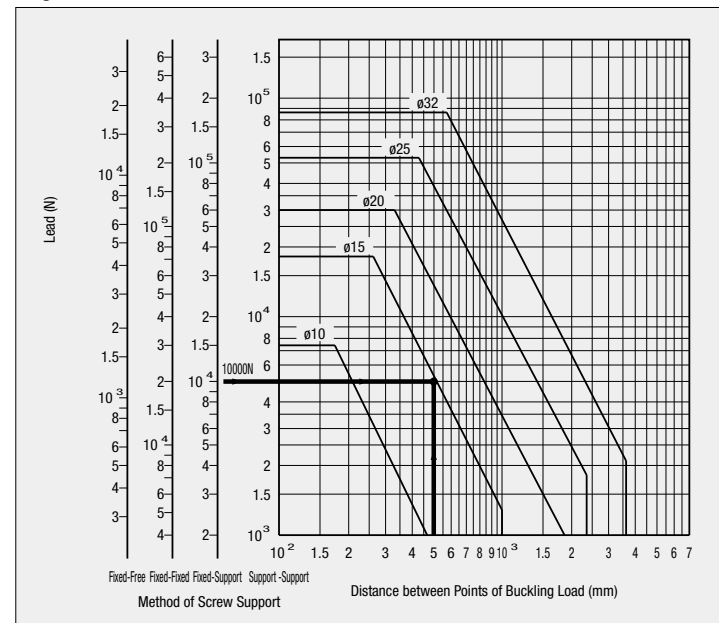
$$P = m \frac{d^4}{\ell^2} \times 10^4 = 10 \times \frac{12.5^4}{820^2} \times 10^4 = 3630(\text{N})$$

Therefore, the rotational speed will need to be 3024rpm or less.

Table.1



•Figure1. Allowable Axial Load Curve



### Screw Shaft Dia. Calculation Example

<Requirements>

- Distance between Points of Buckling Load 500mm
- Mounting method Fixed - Support
- the max. axial load 10000N

<Calculations>

- Find the intersection between a distance of 500mm between load acting points and the axial load of 10000N (from the fixed-support graduation). (Figure 1)
- Read the shaft diameter of the diagonal line nearest to the intersection on the outside. The shaft diameter can be a min. 15mm.

## 5. Allowable Rotational Speed

Ball screw rotational speed is determined by required feed speed and the given screw lead, and needs to be less than the Allowable Maximum Rotational Speed. Ball screw rotational speed is evaluated based on the shaft's critical speed and ball recirculation speed limitation DmN value.

### 5-1. Critical Speed

Allowable rotational speed is defined as a speed 80% or less of the Critical Speed where the rotational speed coincides with a natural resonant frequency of the screw shaft. The Allowable Rotational Speed can be obtained by the following formula.

Additionally, approximate Allowable Rotational Speeds can be obtained from Table 2. Allowable Maximum Rotational Speed Graph.

### •Allowable Rotational Speed (rpm)

$$N_c = f_a \frac{60\lambda^2}{2\pi\ell^2} \sqrt{\frac{EI \times 10^3}{\gamma A}} = g \frac{d}{\ell^2} 10^7 (\text{min}^{-1})$$

Where:

ℓ: Distance of Supports (mm)

f<sub>a</sub>: Safety Factor (0.8)

E: Young's Modulus (2.06×10<sup>11</sup>N/mm<sup>2</sup>)

I: Min. Geometrical Moment of Inertia of Across Root Thread Area (mm<sup>4</sup>)

$$I = \frac{\pi}{64} d^4$$

d: Thread Root Diameter (mm)

γ: Specific Gravity (7.8×10<sup>-6</sup>kg/mm<sup>3</sup>)

A: Root Thread Section Area (mm<sup>2</sup>)

$$A = \frac{\pi}{4} d^2$$

g, λ: Coefficient Determined by Method of Screw Support

Method of Screw Support	g	λ
Support - Support	9.7	π
Fixed - Support	15.1	3.927
Fixed - Fixed	21.9	4.73
Fixed- Free	3.4	1.875

### Allowable Rotational Speed Calculation Example

Find the Allowable Maximum Rotational Speed for Fig.2

<How to use>

- Thread shaft diameter Ø15, Lead 5
- Mounting method Fixed - Support
- Distance between Points of Buckling Load ℓ: 790mm

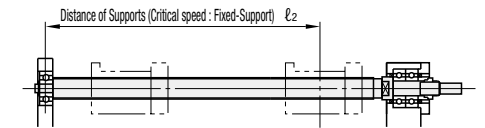
<Calculations>

g=15.1 since the mounting method is Fixed-Supported, the Allowable Rotational Speed (Nc) is,

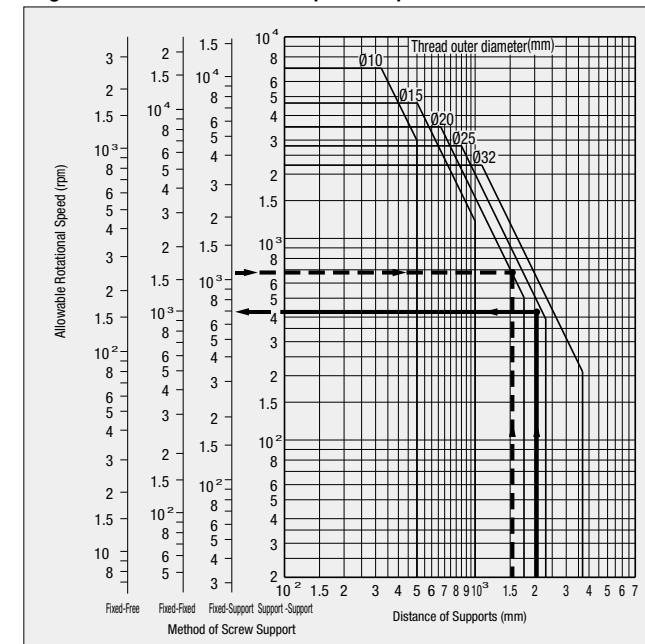
$$N_c = g \frac{d}{\ell^2} 10^7 (\text{rpm}) = 15.1 \times \frac{12.5}{790^2} \times 10^7 (\text{rpm}) = 3024(\text{rpm})$$

Therefore, the rotational speed will need to be 3024rpm or less.

Table.2



•Figure2. Allowable Rotational Speed Graph



### Allowable Rotational Speed Calculation Example

<Requirements>

- Thread outer diameter 20
- Distance of Supports 1500mm
- Mounting method Fixed - Support

<Calculations>

- From Table 2., find an intersection of a vertical line from Supported Span Distance 1500mm and Screw Shaft O.D. Ø20 line.
- The value 1076rpm on the Fixed-Supported scale (Y-Axis) that corresponds to the intersection of (1) above is the Allowable Maximum Speed.

### Screw Shaft Dia. Calculation Example

<Requirements>

- Distance of Supports 2000mm
- Maximum Rotational Speed 1000rpm
- the max. axial load Fixed - Fixed

<Calculations>

- From Table 2., find an intersection of a vertical line from Supported Span Distance 2000mm and a horizontal line from Fixed-Fixed max. speed scale (Y-Axis) at 1000rpm.
- A line that reaches down to the intersection in (1) is the Ø25 ball screw that satisfies the required speed of 1000rpm.

### 5-2. DmN Value

The DmN value represents a ball recirculation (orbit) speed limit within a ball nut. If this value is exceeded, the recirculation components will be damaged. The DmN value can be calculated with the following formula.

### •Allowable Rotational Speed (min<sup>-1</sup>)

DmN ≤ 70000 (Precision Ball Screws)		
DmN ≤ 50000 (Rolled Ball Screws)		
Where:	Ball Dia.	A Value
	1.5875	0.3
	2.3812	0.6
	3.175	0.8
Dm: Thread outer diameter (mm)+A Value	4.7625	1.0
N: Maximum Rotational Speed (min <sup>-1</sup> )	6.35	1.8

# [Technical Data] Selection of Ball Screws 3

## 6. Life Span

Ball screw's life is defined as: Total number of rotations, time, or distance where either the ball rolling surfaces or the balls begin to exhibit repetitive stress caused flaking. Ball screw's life can be calculated based on Basic Dynamic Load Rating with the following formula.

### 6-1. Life Hours (Lh)

$$L_h = \frac{10^6}{60N_m} \left( \frac{C}{P_m f_w} \right)^3 \text{ (hrs)}$$

Where:

Lh: Life Span Hours (hrs)

C: Basic Dynamic Load Rating (N)

P<sub>m</sub>: Mean Axial Load (N)

N<sub>m</sub>: Mean Rotational Speed (min<sup>-1</sup>)

f<sub>w</sub>: Work Factor

Impactless Run	f <sub>w</sub> = 1.0~1.2
Normal Run	f <sub>w</sub> = 1.2~1.5
Run with Impact	f <sub>w</sub> = 1.5~2.0

### •Basic Dynamic Load Rating : C

Basic Dynamic Load Rating (C) is defined as: An axial load which a group of same ball screws are subjected and 90% of the specimen will reach 1 million rotations (10<sup>6</sup>) without experiencing any flaking of the rolling surfaces. See product catalog pages for the Basic Dynamic Load Ratings.

\*Setting life span hours longer than what is actually necessary not only requires a larger ball screw, but also increases the price.

In general, the following standards are used for life span hours:

Machine Tools: 20,000hrs	Automatic Control Equipment: 15,000hrs
Industrial Machinery: 10,000hrs	Measuring Instruments: 15,000hrs

\*The basic dynamic load rating that satisfies the set life span hours is expressed by the following formula.

$$C = \left( \frac{60L_h N_m}{10^6} \right)^{\frac{1}{3}} P_m f_w (N)$$

### 6-2. Axial Load

Axial loads that apply on the screw shafts will vary depending on applicable motion profile such as acceleration, constant velocity, and deceleration phases. Following formula can be used.

-Axial Load Formula-

Constant Velocity ··· Axial Load (P<sub>b</sub>) = μWg

Acceleration ··· Axial Load (P<sub>a</sub>) = Wα + μWg

Deceleration ··· Axial Load (P<sub>c</sub>) = Wα - μWg

\* Omit the "μ" for vertical applications.

μ: Linear motion guide friction coefficient (0.02)

W: Load Mass N

g: Gravitational Acceleration 9.8m/s<sup>2</sup>

α: Acceleration (\*) m/s<sup>2</sup>

(\*) Acceleration (α) = (V<sub>max</sub>/t) × 10<sup>-3</sup>

V<sub>max</sub>: Rapid Feed Rate mm/s

t: Acceleration/Deceleration Time s

### 6-3. Formulas for Average Axial Load and Average Rotational Speed

Average Axial Load and Average Rotational Speed are calculated based on proportions of motion profiles.

Average Axial Load and Average Rotational Speed for Motion profiles in Table 1. can be calculated with the formula 2.

[Table 1. Motion Profile] (t<sub>1</sub>+t<sub>2</sub>+t<sub>3</sub>=100%)

Motion Profile	Axial Load	Rotational Speed	Hours Ratio
A	P <sub>1</sub> (N)	N <sub>1</sub> (min <sup>-1</sup> )	t <sub>1</sub> (%)
B	P <sub>2</sub> (N)	N <sub>2</sub> (min <sup>-1</sup> )	t <sub>2</sub> (%)
C	P <sub>3</sub> (N)	N <sub>3</sub> (min <sup>-1</sup> )	t <sub>3</sub> (%)

### [Formula 2. Average Axial Load Calculation]

$$P_m = \left( \frac{P_1^3 N_1 t_1 + P_2^3 N_2 t_2 + P_3^3 N_3 t_3}{N_1 t_1 + N_2 t_2 + N_3 t_3} \right)^{\frac{1}{3}} (N)$$

$$N_m = \frac{N_1 t_1 + N_2 t_2 + N_3 t_3}{t_1 + t_2 + t_3} \text{ (min}^{-1}\text{)}$$

For machine tool applications, max. load (P1) is applicable for the "Heaviest cutting". Regular Load (P2) is for the general cutting conditions, and Minimum Load (P3) is for the non-cutting rapid feeds during positioning moves.

### Life Calculation Example

<Requirements>

Ball Screw Model	BSS1520 (Ø15 Lead 5)
Mean Axial Load P <sub>m</sub>	250N
Mean Rotational Speed N <sub>m</sub>	2118 (min <sup>-1</sup> )
Work Factor f <sub>w</sub>	1.2

<Calculations>

Since Basic Dynamic Load Rating C for BSS1520 is 4400N,

$$L_h = \frac{10^6}{60 \times 2118} \left( \frac{4400}{250 \times 1.2} \right)^3 = 24824 \text{ (hr)}$$

Therefore, Life will be 24824 hours.

## 7. Screw Shaft Mounting Arrangements

Representative ball screw mounting arrangements are shown below.

Mounting Methods	Application Example
	<ul style="list-style-type: none"> <li>Typical method</li> <li>Medium~High Speeds</li> <li>Medium~High Accuracy</li> <li>For Support Units, Standard Type BRW / BUR is selected.</li> </ul>
	<ul style="list-style-type: none"> <li>Medium Speeds</li> <li>High Accuracy</li> <li>For Support Units, Standard Type BRW is selected.</li> </ul>
	<ul style="list-style-type: none"> <li>Low Speeds</li> <li>For Short Screw Shafts</li> <li>Medium Accuracy</li> <li>For Support Units, Economy Type BRWE is selected</li> </ul>

## 8. Temperature and Life

When ball screws are continuously used at 100°C or higher, or used momentarily at very high temperatures, Basic Dynamic/Static Load Ratings will be reduced according to the temperature rise due to changes in material compositions.

However, there will be no effects up to 100°C. Basic Dynamic Load Rating C" and Basic Static Load Rating Co" at 100°C or higher with the temperature factors ft and ft' can be expressed with the following formula.

$$C'' = f_t C (N)$$

$$Co'' = f_t' Co (N)$$

Temperature °C	100 or less	125	150	175	200	225	250	350
ft	1.0	0.95	0.90	0.85	0.75	0.65	0.60	0.50
ft'	1.0	0.93	0.85	0.78	0.65	0.52	0.46	0.35

For high temperature applications, the current grease should be replaced with the heat-resistant type and the current components should be checked for the heat resistant temperature.

## 9. Rigidity

To improve positioning accuracy and control response of a machine, considerations must be given to the rigidity of feed screw elements. Rigidity (K) of feed screw system can be expressed with the following formula.

$$K = \frac{P}{\delta} \text{ (N/}\mu\text{m)}$$

Where:

P: Axial Loads Applied on Feed Screw System (daN)

δ: Elastic Deformation of Feed Screw System (μm)

Additionally, the following relationship exists between the feed screw system rigidity and other various construction element rigidity.

$$\frac{1}{K} = \frac{1}{K_\epsilon} + \frac{1}{K_n} + \frac{1}{K_b} + \frac{1}{K_h}$$

Where:

K<sub>ε</sub>: Screw Shaft Compressive, Tensile Rigidity

K<sub>n</sub>: Nut Rigidity

K<sub>b</sub>: Support Bearing Rigidity

K<sub>h</sub>: Nut and Bearing Mount Rigidity

### •Screw Shaft Compressive/Tensile Rigidity : K<sub>ε</sub>

$$K_\epsilon = \frac{P}{\delta_\epsilon} \text{ (N/}\mu\text{m)}$$

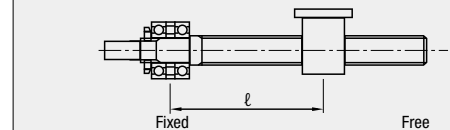
Where:

P: Axial Load (N)

δ<sub>ε</sub>: Screw Shaft Expansion/Contraction (μm)

The expansion and contraction are expressed in the following formula. The expansion and contraction will directly appear as ball screw backlash.

### (1) Fixed-Free Arrangement



$$\delta_\epsilon = \frac{4P\ell}{E\pi d^2} \times 10^3 \text{ (}\mu\text{m)}$$

Where:

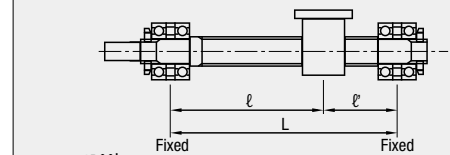
P: Axial Load (N)

E: Young's Modulus (2.06x10<sup>11</sup>N/mm<sup>2</sup>)

d: Screw Shaft Root Diameter (mm)

ℓ: Load Applicable Span Distance (mm)

### (2) Fixed-Fixed Arrangement



$$\delta_\epsilon = \frac{4P\ell\ell'}{E\pi d^2 L} \times 10^3 \text{ (}\mu\text{m)}$$

Where:

P: Axial Load(N)

E: Young's Modulus (2.06x10<sup>11</sup>N/mm<sup>2</sup>)

d: Screw Shaft Root Diameter (mm)

ℓ, ℓ': Load Applicable Span Distance (mm)

L: Mounting Span Distance (mm)

The formula produces the max. value when ℓ = ℓ' =  $\frac{L}{2}$

$$\left( \delta_\epsilon = \frac{PL}{E\pi d^2} \times 10^3 \right)$$

Therefore, the max. shaft expansion and contraction will be 1/4 of Fixed-Free arrangement.

# [Technical Data] Selection of Ball Screws 4

## 10. Driving Torque

This selection provides a guide for selecting ball screw frictional properties and the driving motor.

### 10-1. Friction and Efficiency

When the friction coefficient is  $\mu$ , and lead angle is  $\beta$ , ball screw's efficiency  $\eta$  is indicated by the following formulas.

When rotational force is converted into axial force (Forward Action)

$$\eta = \frac{1 - \mu \tan \beta}{1 + \mu / \tan \beta}$$

When axial force is converted into rotational force (Reverse Action)

$$\eta' = \frac{1 - \mu / \tan \beta}{1 + \mu \tan \beta}$$

### 10-2. Load Torque

The load torque (constant velocity torque) required for the drive power source (motor, etc.) selection is as follows.

#### (1) Forward Action

Torque required when converting rotational force into axial force

$$T = \frac{PL}{2\pi\eta} \quad (\text{N} \cdot \text{cm})$$

Where:

- T: Load Torque (N·cm)
- P: External Axial Load (N)
- L: Ball Screw Lead (cm)
- $\eta$ : Ball Screw Efficiency (0.9)

#### (2) Reverse Action

External axial load when converting axial force into rotational

$$P = \frac{2\pi T}{\eta L} \quad (\text{N})$$

Where:

- P: External Axial Load (N)
- T: Load Torque (N·cm)
- L: Ball Screw Lead (cm)
- $\eta$ : Ball Screw Efficiency (0.9)

#### (3) Friction Torque Caused by Preloading

This is a torque generated by preloading. As external loads increase, the preload of the nut is released and therefore the friction torque by preloading also decreases.

Under No load

$$T_P = K \frac{P_L L}{2\pi} \quad (\text{N} \cdot \text{cm})$$

$$K = 0.05(\tan \beta)^{-\frac{1}{2}}$$

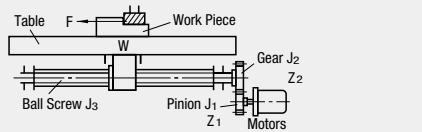
Where:

- $P_L$ : Preload (N)
- L: Ball Screw Lead (cm)
- K: Coefficient of Internal Friction
- $\beta$ : Lead Angle  $\beta = \tan^{-1} \left( \frac{L}{\pi D} \right)$
- D: Thread Outer Diameter

## 11. Selecting the Driving Motors

When selecting a driving motor, it is necessary to satisfy the following conditions:

1. Ensure a marginal force sufficient to counter the load torque exerted on the motor's output thread.
2. Enable starting, stopping at prescribed pulse speeds, sufficiently powered to counter the moment of inertia exerted on the motor's output thread.
3. Obtain the prescribed acceleration and deceleration constants, sufficient to counter the moment of inertia exerted on the motor's output thread.



#### (1) Constant Speed Torque Exerted on the Motor Output Thread

This is the amount of torque required to drive the output thread against the applied external load, at a constant speed.

$$T_1 = \left( \frac{PL}{2\pi\eta} + T_P \frac{(3PL-P)}{3PL} \right) \frac{Z_1}{Z_2} \quad (\text{N} \cdot \text{cm})$$

Where:  $P \leq 3PL$

- $T_1$ : Driving Torque at Constant Speed (N·cm)
- P: External Axial Load (N)
- $P = F + \mu Mg$
- F: Thrust Reaction Produced in Cutting Force (N)
- M: Masses of Table and Work Piece (kg)
- $\mu$ : Coefficient of Friction on Sliding Surfaces
- g: Gravitational Acceleration (9.8m/s<sup>2</sup>)
- L: Ball Screw Lead (cm)
- $\eta$ : Mechanical Efficiency of Ball Screw or Gear
- $T_P$ : Friction Torque Caused by Preloading (N·cm) Refer to Formula 10-2-(3)
- $P_L$ : Preload (N)
- $Z_1$ : Number of Pinion's Teeth
- $Z_2$ : No. of Gear's Teeth

#### (2) Acceleration Torque Exerted on the Motor Output Thread

This is the amount of torque required to drive the output shaft against the external load during acceleration.

$$T_2 = J\omega = J\frac{2\pi N}{60t} \times 10^{-3} \quad (\text{N} \cdot \text{cm})$$

$$J = J_1 + J_4 + \left( \frac{Z_1}{Z_2} \right)^2 \left\{ J_2 + J_3 + J_5 + J_6 \right\} \quad (\text{kg} \cdot \text{cm}^2)$$

Where:

- $T_2$ : Driving Torque in Acceleration (N·cm)
- $\omega$ : Motor Thread Angular Acceleration (rad/s<sup>2</sup>)
- N: Motor Thread Rotational Speed (rpm)
- t: Acceleration Time (s)
- $J$ : Moment of Inertia Exerted on the Motor (kg·cm<sup>2</sup>)
- $J_1$ : Moment of Inertia Exerted on Pinion (kg·cm<sup>2</sup>)
- $J_2$ : Moment of Inertia Exerted on Gear (kg·cm<sup>2</sup>)
- $J_3$ : Moment of Inertia Exerted on Ball Screw (kg·cm<sup>2</sup>)
- $J_4$ : Moment of Inertia Exerted on Motor's Rotor (kg·cm<sup>2</sup>)
- $J_5$ : Moment of Inertia of Moving Body (kg·cm<sup>2</sup>)
- $J_6$ : Moment of Inertia of Coupling (kg·cm<sup>2</sup>)
- M: Masses of Table and Work Piece (kg)
- L: Ball Screw Lead (cm)

Moment of inertia exerted on cylinders as screws and cylinders such as Gears (Calculation of  $J_1 \sim J_4, J_6$ )

$$J = \frac{\pi \gamma}{32} D^4 \ell \quad (\text{kg} \cdot \text{cm}^2)$$

Where:

- D: Cylinder Outer Diameter (cm)
- $\ell$ : Cylinder Length (cm)
- $\gamma$ : Material Specific Gravity  $\gamma = 7.8 \times 10^{-3}$  (kg/cm<sup>3</sup>)
- $J_5 = M \left( \frac{L}{2\pi} \right)^2$  (kg·cm<sup>2</sup>)

#### (3) Total Torque Exerted on the Motor Output Thread

Overall torque can be obtained by adding results from formulas (1) and (2).

$$T_M = T_1 + T_2 = \left( \frac{PL}{2\pi\eta} + T_P \frac{(3PL-P)}{3PL} \right) \frac{Z_1}{Z_2} + J\frac{2\pi N}{60t} \times 10^{-3} \quad (\text{N} \cdot \text{cm})$$

Where:

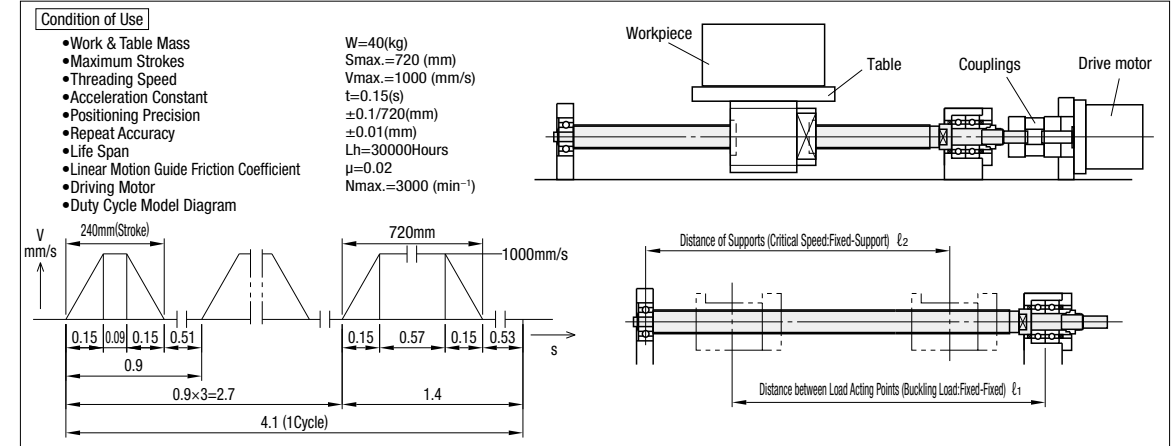
- $T_M$ : Total Torque Exerted on the Motor Output Thread (N·cm)
- $T_1$ : Driving Torque at Constant Speed (N·cm)
- $T_2$ : Driving Torque at In Acceleration (N·cm)

Once you have temporarily found the type of motor you need, check

1. effective torque,
2. acceleration constant and
3. motor overload properties and heat tolerance during repeated starting, stopping.

It is necessary to ensure a sufficient margin for these parameters.

## 12. Example of Selection of Ball Screws (in case of X-axis)



### 1. Setting Lead (L)

Set lead based on maximum motor revolutions and threading speed. Use the following formula.

$$L \geq \frac{V_{\max} \times 60}{N_{\max}} = \frac{1000 \times 60}{3000} = 20 \text{ (mm)}$$

Required lead is 20mm or higher.

### 2. Nut selection

#### (1) Calculating Axial Load

The axial load calculation formula on Clause 6-2, P2227 is used to calculate the axial loads for each segment of a motion profile.

- At Constant Speed  
Axial Load (Pb) =  $\mu Wg = 0.02 \times 40 \times 9.8 = 8$  (N)
- In Acceleration  
Acceleration (a) =  $(V_{\max}/t) \times 10^{-3} = (1000/0.15) \times 10^{-3} = 6.67$  (m/s<sup>2</sup>)  
Axial Load (Pa) =  $Wg + \mu Wg = 40 \times 6.67 + 0.02 \times 40 \times 9.8 = 274$  (N)
- In Deceleration  
Axial Load (Pc) =  $Wg - \mu Wg = 40 \times 6.67 - 0.02 \times 40 \times 9.8 = 260$  (N)

#### (2) Actual moving time during each segment in a motion profile

Below derived from Duty Cycle Model Diagram.

Operating Pattern	In Acceleration	At Constant Speed	In Deceleration	Total Operating Time
Operating Time	0.60	0.84	0.60	2.04

#### (3) Summary of Axial Loads, Rotational Speeds, and Operation Time for Each Motion Profile

Operating Pattern	In Acceleration	At Constant Speed	In Deceleration
Axial Load	274N	8N	260N
Rotational Speed	1500min <sup>-1</sup>	3000min <sup>-1</sup>	1500min <sup>-1</sup>
Operating Time Ratio	29.4%	41.2%	29.4%

#### (4) Calculating the Average Axial Load with a formula in P2227, 6-3.

$$\text{Mean Axial Load (Pm)} = \left( \frac{P_1^3 N_1 t_1 + P_2^3 N_2 t_2 + P_3^3 N_3 t_3}{N_1 t_1 + N_2 t_2 + N_3 t_3} \right)^{\frac{1}{3}} = 200 \text{ (N)}$$

#### (5) Calculating the mean turns

$$\text{Mean Turns (Nm)} = \frac{N_1 t_1 + N_2 t_2 + N_3 t_3}{t_1 + t_2 + t_3} = 2118 \text{ (min}^{-1}\text{)}$$

#### (6) Calculation of the required basic dynamic load rating

##### (1) Calculating Continuous Operational Life (Lho)

A Continuous Operational Life which is derived by subtracting Resting time from Desired Life while a motion profile of 4.01s with a moving time of 2.04s can be calculated as follows.

$$L_{ho} = \text{Desired Life (Lh)} \times \left( \frac{2.04}{4.1} \right) = 14927 \text{ (Hours)}$$

##### (2) Calculating Required Basic Dynamic Load Rating

The formula on Clause 6-1, P2227 is used to calculate the basic dynamic load rating required to retain the net operational life of ball screw.

$$C = \left( \frac{60 L_{ho} N_m}{10^6} \right)^{\frac{1}{3}} \times P_m \times f_w = \left( \frac{60 \times 14927 \times 2118}{10^6} \right)^{\frac{1}{3}} \times 200 \times 1.2 = 2970 \text{ (N)}$$

##### (7) Tentative Ball Screw Selection

A ball screw to satisfy the requirements of Lead 20 and Basic Dynamic Load Rating of 2970N, BSS1520 is tentatively selected.

### 3. Accuracy Evaluation

#### (1) Evaluating Accuracy Grades and Axial Clearances

By referencing the "Ball Screw Lead Accuracy" table on Section 2., P2223, it is found that the Accuracy Grade C5 with  $\pm 0.040 / 800 \sim 1000$ m of actual mean travel error satisfies the positioning accuracy:  $\pm 0.1/720$ mm and therefore, that BSS1520 is fully applicable.

Additionally, the Precision Screws axial clearance table on P2224 shows that axial clearance of BSS1520 is 0.005 or less. The required positioning repeatability is  $\pm 0.01$ mm, and it can be confirmed that BSS1520 satisfies the requirement.

### 4. Screw Shaft Selection

#### (1) Determining the Overall Length

Screw Shaft O.A.L. (L) = Max. Stroke + Nut Length + Margin + Shaft End Terminations (both sides). Therefore,

Max Stroke: 720mm  
Nut Length: 62mm  
Margin: Lead  $\times 1.5 = 60$ mm  
Shaft End Termination Dims.: 72

Screw Shaft O.A.L. (L) = 720 + 62 + 60 + 72 = 914 (mm)

\* The Margin is provided as a countermeasure against overruns, and the amount is typically set as 1.5~2 times as much as the screw lead. Lead  $20 \times 1.5 \times 2$  (Both Ends) = 60 (mm)

#### (2) Evaluating the Allowable Axial Load

Load Applicable Span Distance  $\ell_1$  is 820mm, and the Axial Load can be obtained by the formula on P2225, "4. Allowable Axial Load" as indicated below.

$$P = m \frac{d^4}{\ell^2} = 10 \times \frac{12.5^4}{820^2} \times 10^4 = 3660 \text{ (N)}$$

The above formula produces an Axial Load value of 343N which is well within the Allowable Max. Axial Load 3660N, and suitability is confirmed.

#### (3) Evaluating the Allowable Max. Rotational Speed

Shaft supported span is 790mm, and the Critical Speed  $N_c$  value is calculated as follows by using the formula on "5-1. Critical Speed" in P2226:

$$N_c = g \frac{d}{\ell^2} = 15.1 \times \frac{12.5}{790^2} \times 10^7 = 3024 \text{ (min}^{-1}\text{)}$$

The max. speed requirement of 3000rpm is within the Critical Speed of 3024min<sup>-1</sup>, and the suitability is confirmed.

Additionally, the DmN value can be calculated by using the formula in P2226, "5-2. DmN Value" as:

$$DmN = (\text{Shaft O.D.} + A \text{ value}) \times \text{Max Rotational Speed} = 15.8 \times 3000 = 47400 \leq 70000$$

and the suitability is confirmed.

### 5. Selection Result

From the above, it is determined that a suitable ball screw model is BSS1520-914.